## REMARKS

Claims 9-23 were rejected under 35 U.S.C.§102(b) as being anticipated by Hirota et al.(Hirota).

Reconsideration is requested.

The glass disclosed by Hirota contains 5 - 12wt.% of Li<sub>2</sub>O for lowering the sag point without causing the chemical durability to deteriorate (col. 5, line 38). The amount of Li<sub>2</sub>O in Example 10 of the Hirota patent is 7.3wt.%. In contrast, the glass of the present invention may include 0-3mass% of Li<sub>2</sub>O in order to enhance the melting properties.

The amended claims point out a glass having the property of having a very small variation in the refractive index which is caused by the compaction phenomenon. For these reasons, the amended claims are not anticipated by Hirota and withdrawal of this ground of rejection is requested.

Claims 9-38 were rejected under 35 U.S.C.§102(b) as being anticipated by Danielson et al. (Danielson)

The Danielson patent discloses a glass composition having 5.6 - 11% of Al<sub>2</sub>O<sub>3</sub> in the specification and 4 - 8% in the claims. In col. 2, lines 4-8 of Danielson, it was disclosed that increased fluoride release is observed in glasses with a lower Al<sub>2</sub>O<sub>3</sub> content and therefore, the glasses will contain no more than about 8wt% of Al<sub>2</sub>O<sub>3</sub>. The amended claims of the present application point out that the Al<sub>2</sub>O<sub>3</sub> content is a maximum of 2.3 mass % as disclosed in Example 25 which clearly distinguishes the claimed invention from the Danielson patent. The Al<sub>2</sub>O<sub>3</sub> is added to the glass composition to improve the chemical durability and to adjust the viscosity of the glass and the refractive index. A Table is attached which shows the relationship between the weight % of Danielson and the conversion to mass % in order to allow a comparison of the Danielson patent with the claims of the present application. For these reasons, the amended claims of the present application are clearly distinguishable from the Danielson patent and it is requested that this ground of rejection be withdrawn.

Claims 9-11, 14-156, 19-21, 24-26 and 34-36 were rejected under 35 U.S.C.§102(b) as being anticipated by Kasori et al. (Kasori).

Reconsideration is requested.

Kasori discloses a optical fiber for optical communication. The patentee disclosed a composition for a glass fiber core and a composition for a glass fiber clad layer. In the core glass composition, 3 - 7wt.% of Al<sub>2</sub>O<sub>3</sub> added to inhibit devitrification and improve water resistance. If the level of Al<sub>2</sub>O<sub>3</sub> is lower than 3wt.%, no improvement in water resistance can be recognized and the glass is subject to devitrification. The composition of the glass fiber clad layer Al<sub>2</sub>O<sub>3</sub> is added in an amount of 4 - 7wt%. At col. 3, lines 65- col. 4, line 1, the patentee teaches that the Al<sub>2</sub>O<sub>3</sub> has no effect at a level of less than 4wt.%. For this reason, there is no motivation in Kasori to use less than 4wt.% of Al<sub>2</sub>O<sub>3</sub>. Kasori discloses samples 1, 2, 9, 26,

and 27 as having Al<sub>2</sub>O<sub>3</sub> at a level of less than 2.3wt% but these samples all contain CaO at a level of 3.55wt% which are excluded from the amended claims of the present application which specify a maximum of no more than 2wt.% of CaO. For these reasons, the amended claims of the present application are not anticipated by Kasori and it is requested that this ground of rejection be withdrawn.

Claims 9-38 were rejected under 35 U.S.C.\\$102(b) as being anticipated by Faulstich.

Reconsideration is requested.

The Faulstich patent discloses an optical glass having an nd of 1.650±2X10<sup>-3</sup> and vd of 55.5±1.0 which contains SiO<sub>2</sub> in an amount ranging from 32.5 - 33.5wt%. This patent does not disclose why the amount of the SiO<sub>2</sub> is limited. The amended claims of the present application point out that the amount of the SiO<sub>2</sub> is from 55.35 to 70mass%. The lower limit of 55.35mass% is based on Example 27 In addition, the glasses of all of the Examples of the present invention have an nd of 1.6056 or below and a vd of 58.7 which are outside of the ranges of the optical constants of Faulstich. The Faulstich patent does not disclose or suggest the composition and properties of the glass that is defined by the amended claims of the present application. For these reasons, it is requested that this ground of rejection be withdrawn.

The specification has been amended to delete Examples 28-30, 34, 35 and 38.

An early and favorable action is earnestly solicited.

Respectfully submitted,

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|        |       | 15      | 16      | 17      | 18      | 19      | 20      | 21      | 22      | 23      | 29      | 99      | <u>ب</u> |
|--------|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|
|        | SiO2  | 49.100  | 51.700  | 45.900  | 49.300  | 43.600  | 25.900  | 49.700  | 53.300  | 47.300  | 48.600  | 50.300  | 52.200   |
|        | AI203 | 8.300   | 11.000  | 10.500  | 10.800  | 10.300  | 6.100   | 5.800   | 000'9   | 5.700   | 8.100   | 8.400   | 8.700    |
|        | AIF3  |         |         |         |         |         |         |         |         |         |         |         |          |
|        | B203  | 8.400   | 008'9   | 6.500   | 10.100  | 9.600   | 000'/   | 0.09    | 10.300  | 9.800   | 8.400   | 8.700   | 9.000    |
|        | BaO   | 4.300   |         | 8.300   |         | 8.200   |         | 8.500   |         | 8.300   |         |         |          |
|        | BaF2  | 29.900  | 30.500  | 28.900  | 29.900  | 28.400  | 31.100  | 29.500  | 30.500  | 28.900  | 64.900  | 27.400  | 19,300   |
|        | SrO   |         |         |         |         |         |         |         |         |         |         |         |          |
|        | ZnF2  |         |         |         |         |         |         |         |         |         |         | 5.200   | 10.700   |
|        | total | 100.000 | 100.000 | 100.100 | 100.100 | 100.100 | 100.100 | 100.100 | 100,100 | 100.000 | 130.000 | 100.000 | 99.900   |
|        | mass% |         |         |         |         |         |         |         |         |         |         |         |          |
|        |       | 15      | 16      | 17      | 18      | 19      | 20      | 21      | 22      | 23      | 29      | 8       | 31       |
| 60.08  | Si02  | 47.796  | 50.300  | 44.677  | 47.944  | 42.457  | 54.304  | 48.350  | 51.806  | 46.085  | 35.756  | 48.691  | 50.524   |
| 101.96 | AI203 | 8.080   | 10.702  | 10.220  | 10.503  | 10.030  | 5.926   | 5.642   | 5.832   | 5.554   | 5.959   | 8.131   | 8.421    |
| 69.62  | B203  | 8.177   | 6.616   | 6.327   | 9.822   | 9.348   | 6.800   | 6.421   | 10.011  | 9.548   | 6.180   | 8.422   | 8.711    |
| 153.33 | BaO   | 29.640  | 25.951  | 32.679  | 25.429  | 32.171  | 26.422  | 33.367  | 25.926  | 32.711  | 41.757  | 23.196  | 16.337   |
| 103.62 | SrO   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000    |
| 81.39  | ZnO   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 3.963   | 8.153    |
| 19.00  | u.    | 6.308   | 6.431   | 960.9   | 6.302   | 5.994   | 6.548   | 6.220   | 6.425   | 6.102   | 10.348  | 7.598   | 7.855    |
|        | total | 100 000 | 100 000 | 100 000 | 100 000 | 100 000 | 100000  | 100 000 | 100 000 | 100000  | 100 000 | 100 001 | 10000    |

Danielson conversion of examples (weight %)

(weight %)

|              | 32      | 33      | 34      | 35      | 36      | 37      | 38      | 39      | 40      | 41      | 42      | 43      |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| S:02         | 54.200  | 56.700  | 46.700  | 49.300  | 52.200  | 55.400  | 47.400  | 47.400  | 47.400  | 46.900  | 46.900  | 46.900  |
| A1203        | 9.100   | 9.500   | 5.600   | 5.900   | 6.200   | 0.600   | 8.000   | 8.000   | 8.000   |         |         |         |
| AIF3         |         |         |         |         |         |         |         |         |         | 13.600  | 13.600  | 13.600  |
| B203         | 9.300   | 9.800   | 9.700   | 10.300  | 10.900  | 11.500  | 8.100   | 8.100   | 8.100   | 8.000   | 8.000   | 8.000   |
| BaO          |         |         |         |         |         |         |         |         |         | 29.000  | 29.000  | 29.000  |
| BaF2         | 10.600  |         | 37.900  | 26.800  | 14.000  |         | 33.600  | 33.600  | 33.600  |         |         |         |
| SrO          |         |         |         |         |         |         |         |         |         |         |         |         |
| ZnF2         | 16.700  | 24.100  |         | 7.800   | 16.700  | 26.500  |         |         |         |         |         |         |
| total        | 006.66  | 100.100 | 99.900  | 100.100 | 100.000 | 100.000 | 97.100  | 97.100  | 97.100  | 97.500  | 97.500  | 97.500  |
| mass%        |         |         |         |         |         |         |         |         |         |         |         |         |
|              | 32      | 33      | 34      | 35 '    | 36      | 37      | 38      | 39      | 40      | 41      | 42      | 43      |
| 60.08 SiO2   | 52.392  | 54.609  | 45.182  | 47.517  | 50.259  | 53.218  | 47.321  | 47.321  | 47.321  | 46.259  | 46.259  | 46.259  |
| 101.96 AI2O3 | 8.796   | 9.150   | 5.418   | 5.687   | 5.969   | 6.340   | 7.987   | 7.987   | 7.987   | 8.143   | 8.143   | 8.143   |
| 69.62 B2O3   | 8.990   | 9.439   | 9.385   | 9.927   | 10.495  | 11.047  | 8.087   | 8.087   | 8.087   | 7.891   | 7.891   | 7.891   |
| 3.33 BaO     | 8.961   | 0.000   | 32.068  | 22.590  | 11.788  | 0.000   | 29.336  | 29.336  | 29.336  | 28.603  | 28.603  | 28.603  |
| 103.62 SrO   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   | 0.000   |
| 1.39 ZnO     | 12.708  | 18.273  | 0.000   | 5.918   | 12.658  | 20.040  | 0.000   | 0.000   | 0.000   | 0.000   | 0000    | 0.000   |
| 19.00 F      | .8.153  | 8.531   | 7.947   | 8.361   | 8.831   | 9.356   | 7.270   | 7.270   | 7.270   | 9.104   | 9.104   | 9.104   |
| total        | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 | 100.000 |
|              |         |         |         |         |         |         |         |         |         |         |         |         |